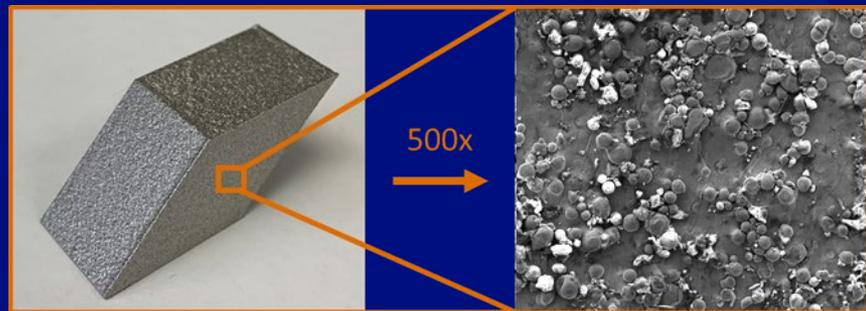


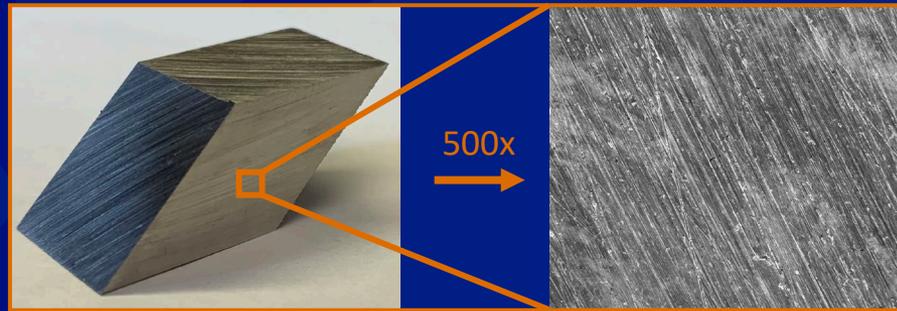
# Pulse/Pulse Reverse Electropolishing of Additively Manufactured 316L Stainless Steel by NaCl/H<sub>2</sub>O

Timothy Gorey, Daniel Hooks, Robert Hackenberg, Courtney Clark, Colt Montgomery, and Jamie Stull



Additive

$S_a = \sim 10-12 \mu\text{m}$



Machined

$S_a = \sim 1 \mu\text{m}$

Can AM materials have a similar finish to machining?

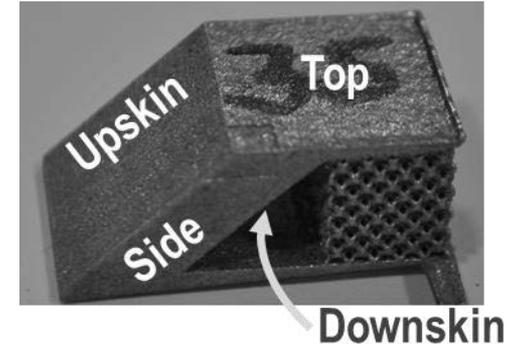
# Metal Additive Manufacturing (MAM) is a powerful capability that can obtain high strength:weight components with complex geometry

## Benefits MAM vs Traditional:

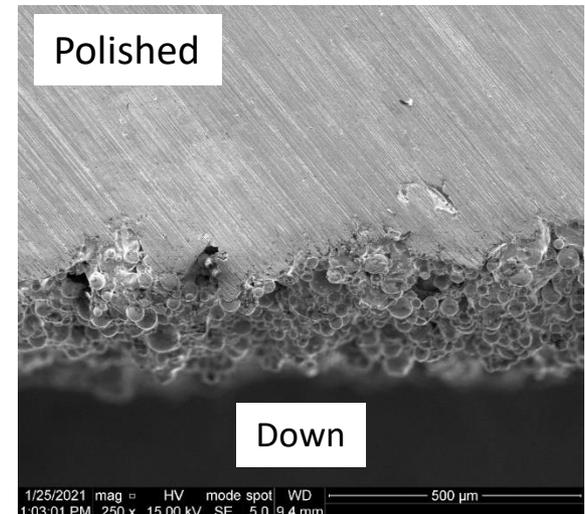
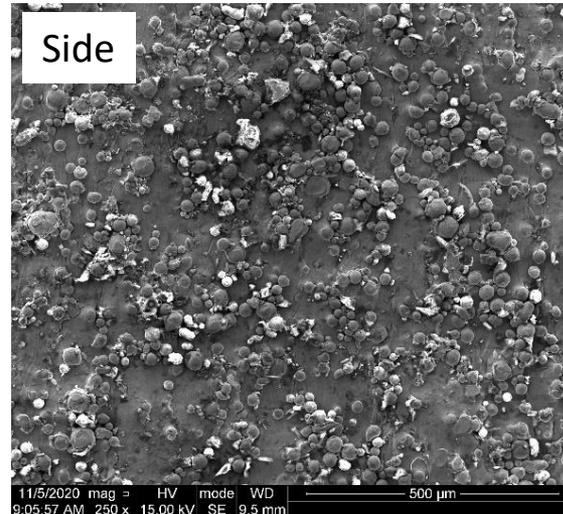
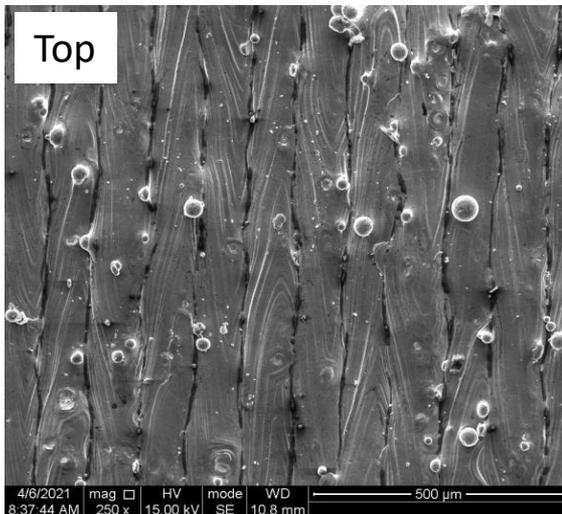
- Production is tightly connected to CAD design.
- High strength originating from complex geometries (e.g. lattices)

## Limitations:

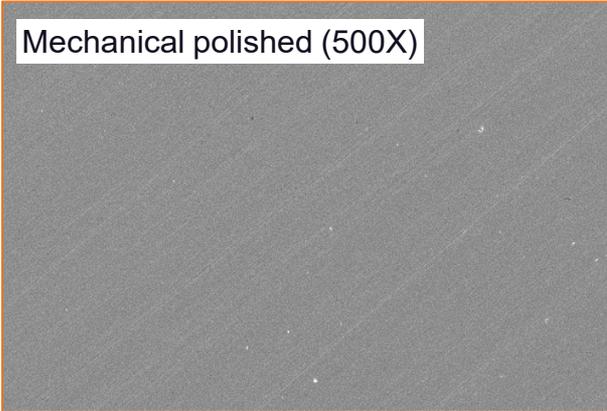
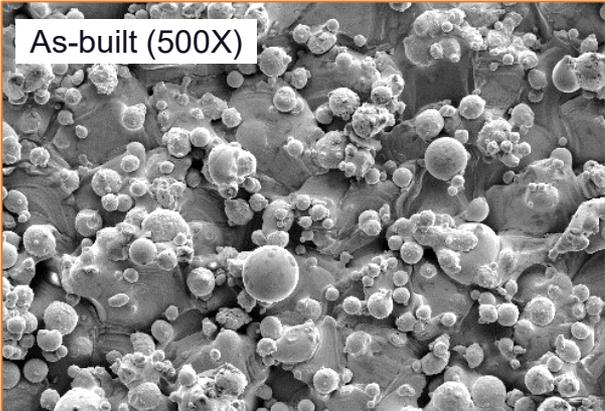
- Manufacturing is outpacing finishing capabilities
- As-built surfaces are rough, due to powder particle size
- Roughness-related issues: tolerance, corrosion
- Finishing solutions are needed for MAM part interchangeability



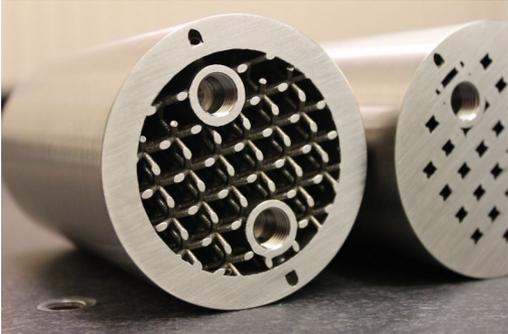
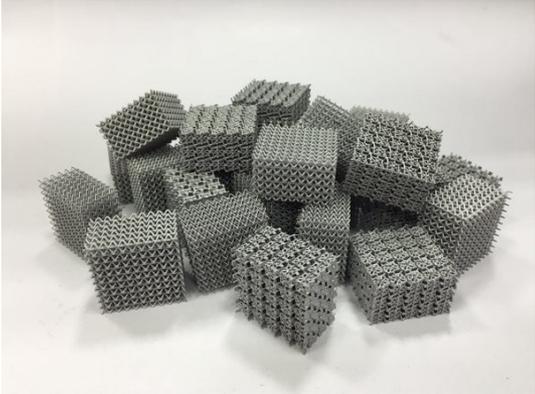
## Microstructure varies with build orientation



# Dealing with Surface Roughness

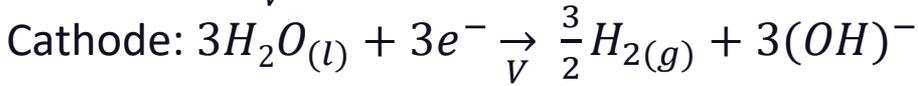
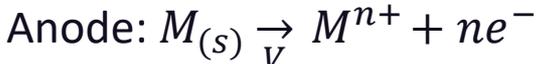
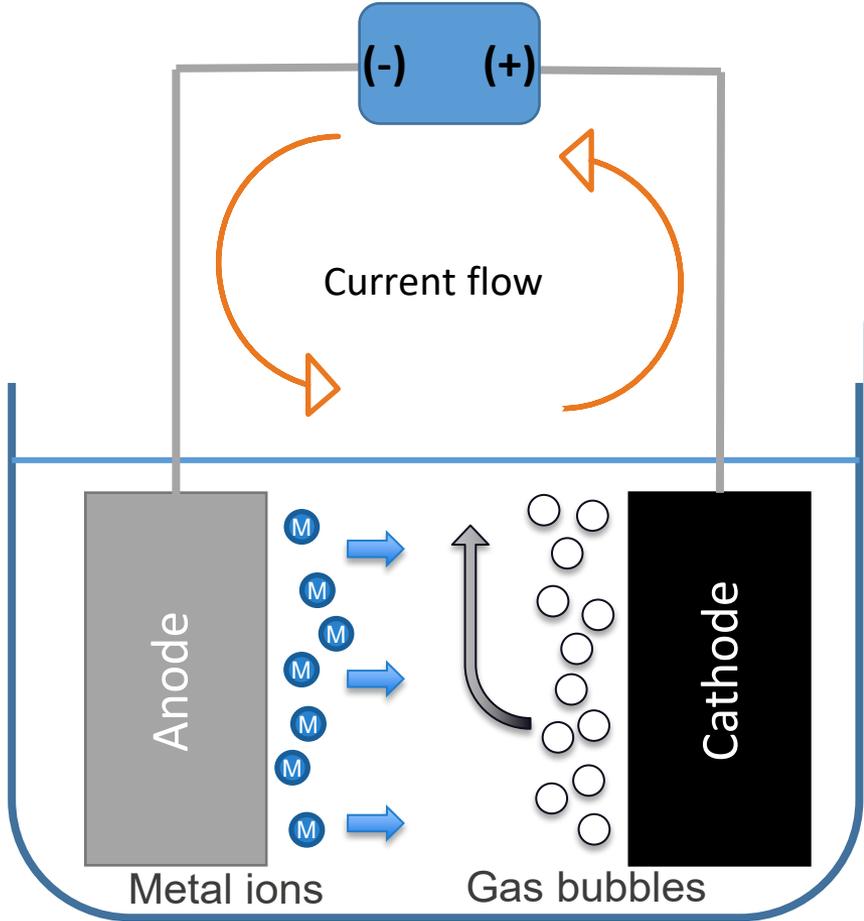
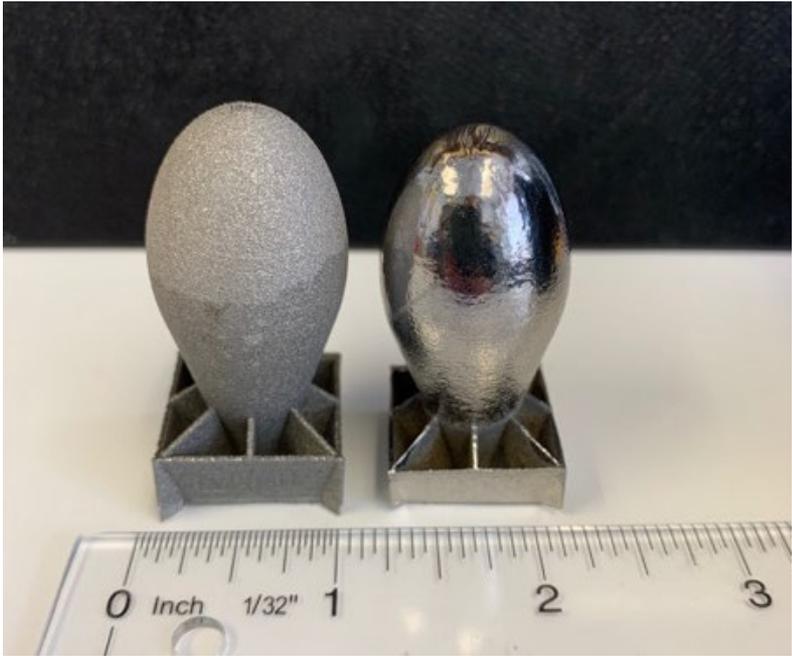


Mechanical polishing is an effective finishing technique, but how do you apply it to components like this?

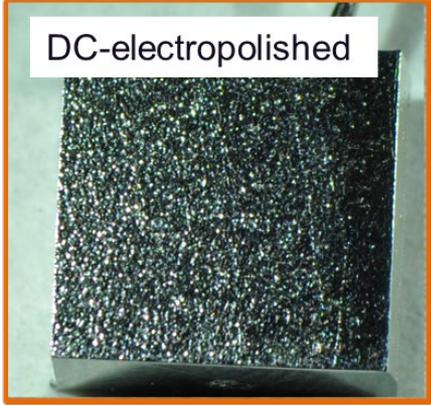
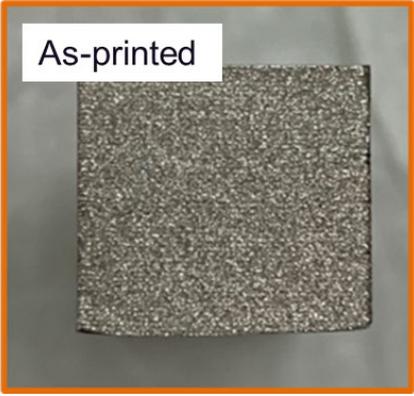


# DC Electropolishing: $H_3PO_4/H_2SO_4$ /Glycerol/HF

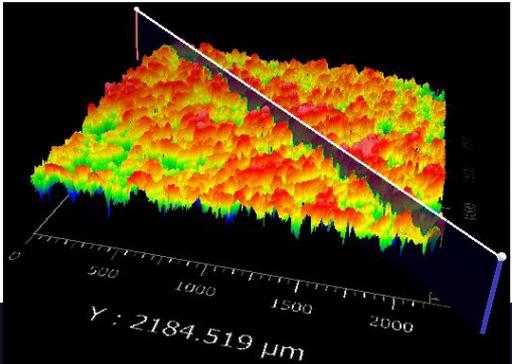
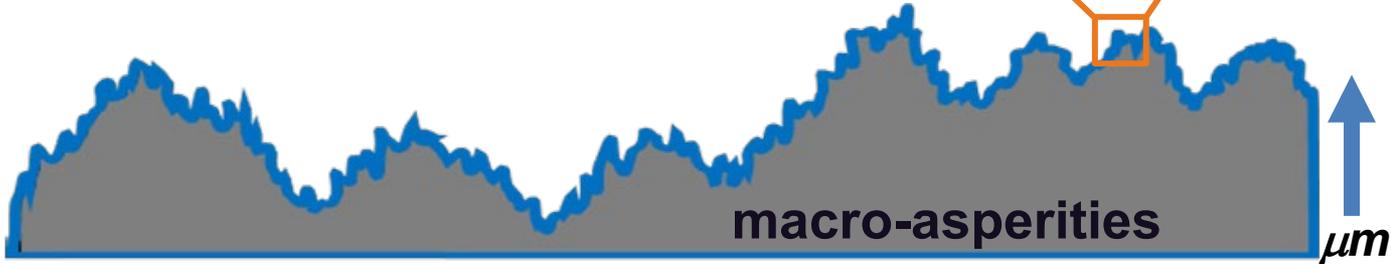
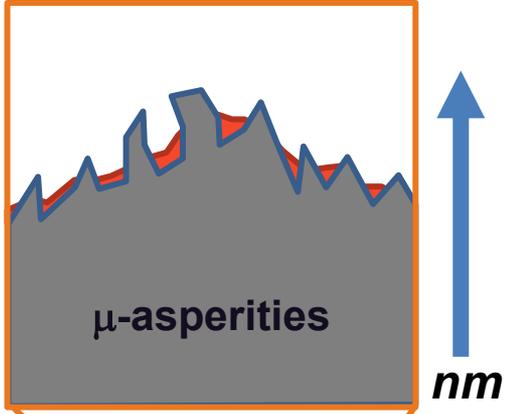
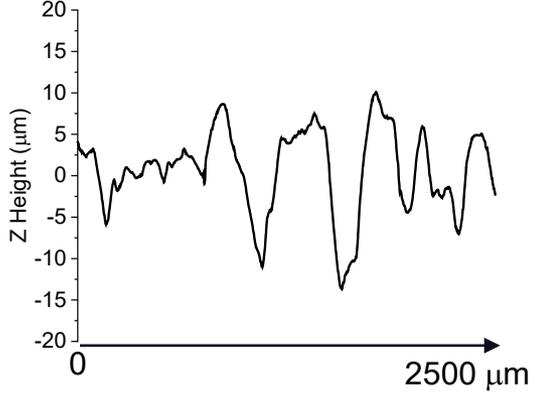
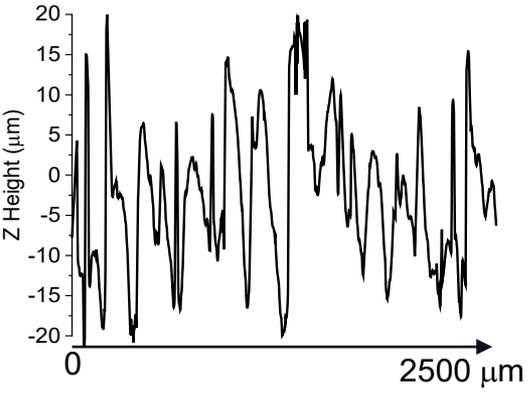
Electropolishing is a good solution for AM:  
Full parts can be submerged, reaching  
internal surfaces



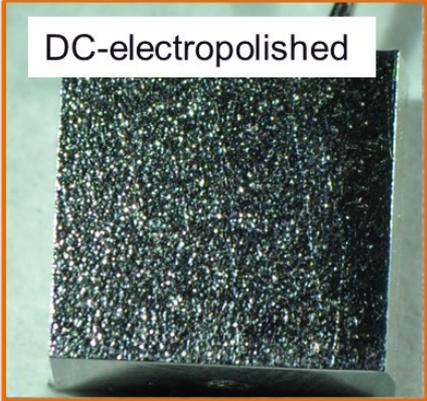
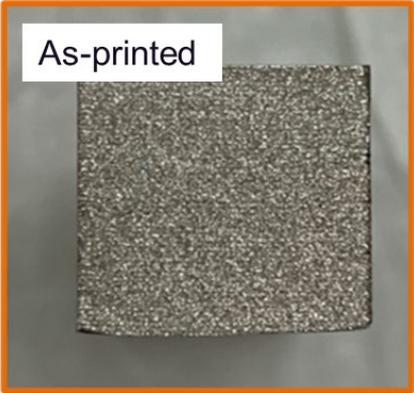
# DC Electropolishing and Surface Roughness



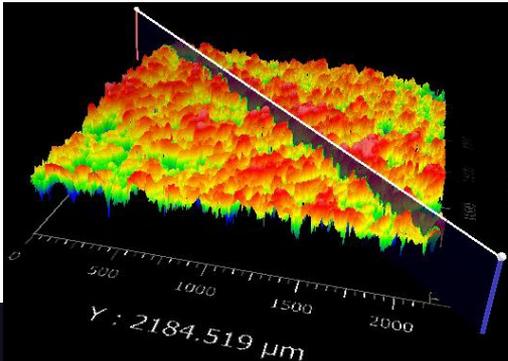
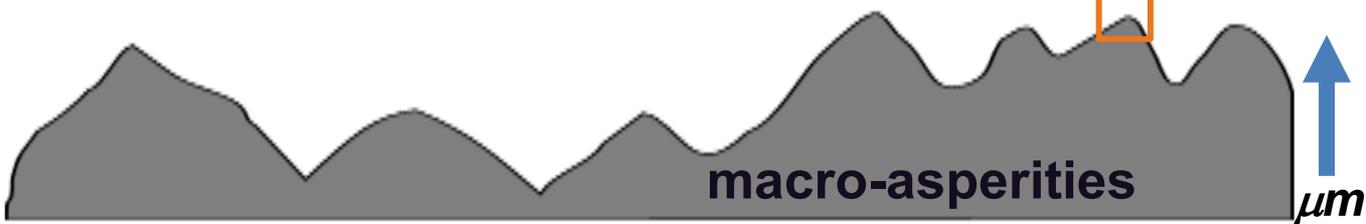
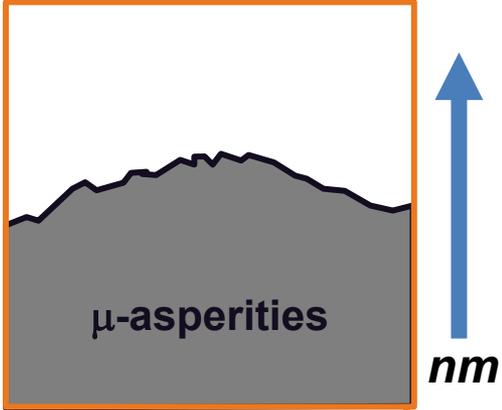
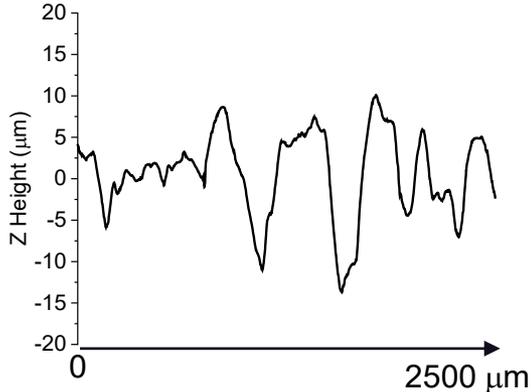
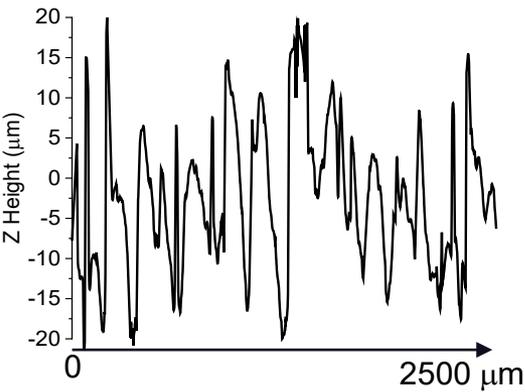
DC method gives a “mirror” finish but can’t smooth macro-asperities



# DC Electropolishing and Surface Roughness



DC method gives a “mirror” finish but can’t smooth macro-asperities



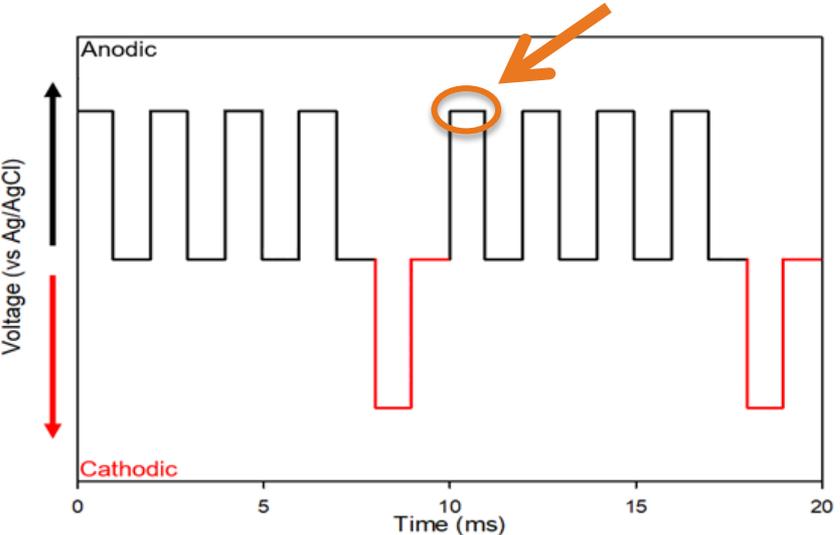
# Pulse/Pulse Reverse Electropolishing

**Hypothesis:**

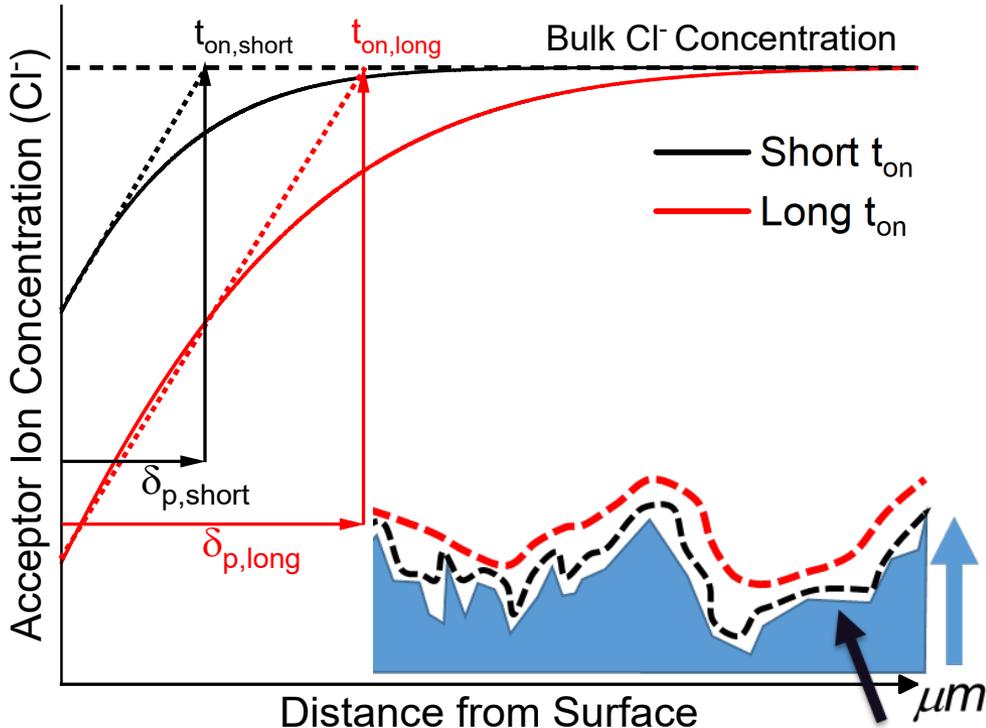
Use any electrolyte: NaCl/Na<sub>2</sub>SO<sub>4</sub> in H<sub>2</sub>O is compatible with dissolved metal

$$\delta_p \approx (2Dt_{on})^{\frac{1}{2}}$$

Depletion/ion layer thickness ( $\delta_p$ ) is controllable with  $t_{on}$



Cathode pulses eliminate need for HF



Cl- depletion under dashed line

Pure diffusion control: no concentrated acids

# Pulse/Pulse Reverse Electropolishing:

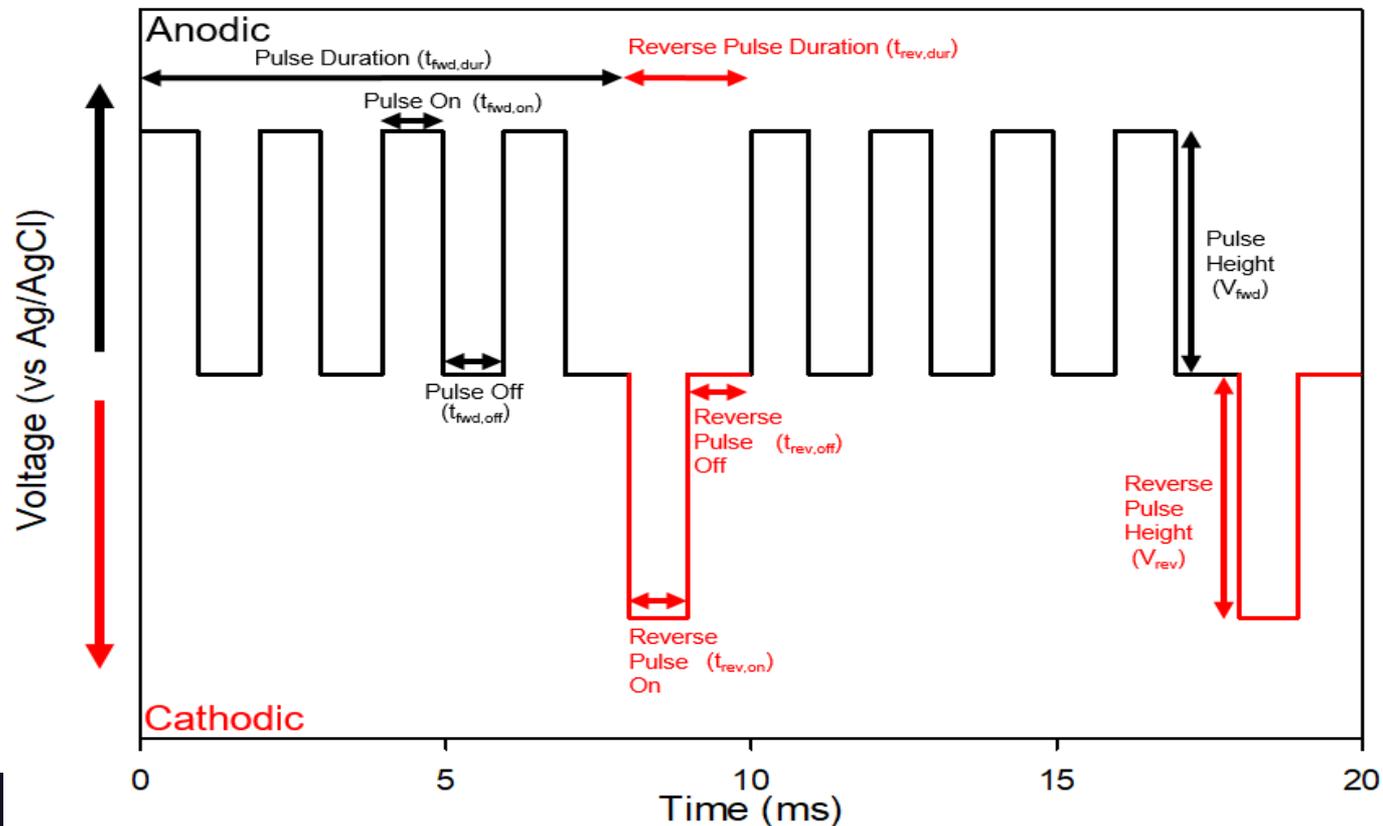
## Summary:

Anodic pulses are sent to the work piece to etch asperities, and intermittent cathodic pulses are applied to depassivate the surface.

## Challenge: high dimensionality

**Solution conditions:** chemical species, temperature, viscosity, resistivity

**Potentiostatic:** pulse on/off time, anodic/cathodic amplitude, duration, anode:cathode pulse ratio.



# Pulse Parameter Experiments:

## Goal:

Independently vary pulse/solution parameters and gauge surface finishing qualitatively (by inspection) and quantitatively (by profilometry).

## Controlled Experiments (key terms):

### 1.) **Effective Current**

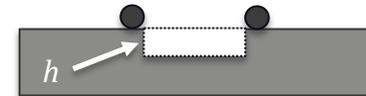
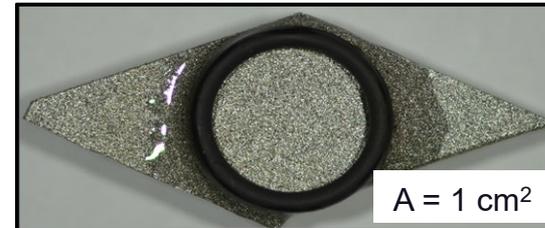
= Current the sample experiences, after accounting for on-times, off-times, and reverse pulses. (essentially an equivalent DC current)

$$\text{Effective Current} = \frac{\text{Ampere}}{\text{cm}^2}$$

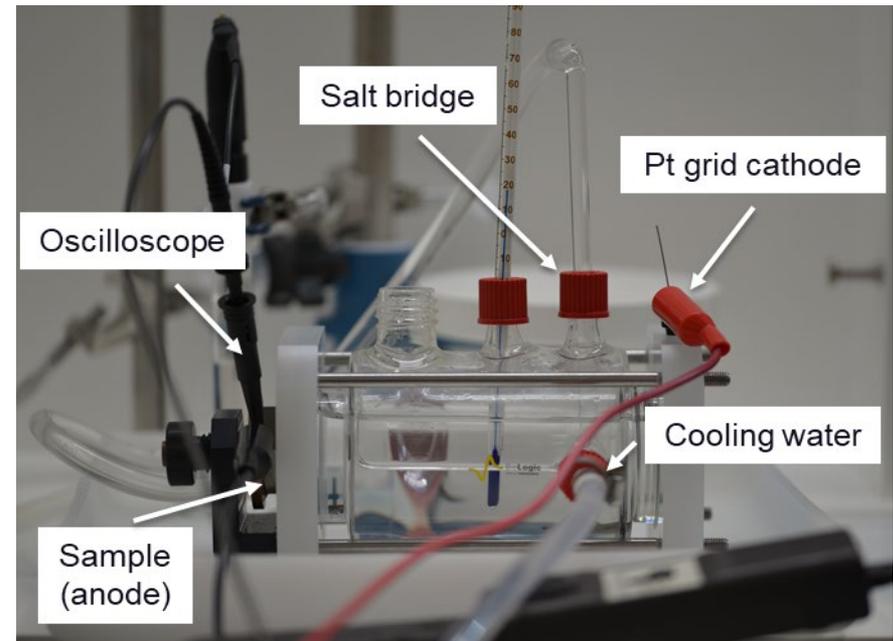
### 2.) **Coulombic Density** (integrated current density)

= Total amount of charge transferred in the electropolishing process.

$$\text{Coulombic Density} = \frac{\text{Ampere} * \text{min}}{\text{cm}^2}$$



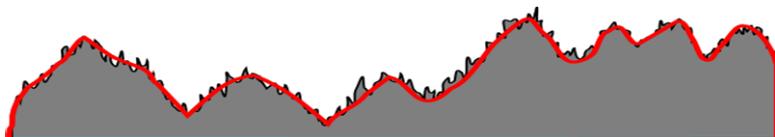
$$V_{\text{dissolved}} = \frac{1 \text{ cm}^3}{7.8429 \text{ g}} \times \Delta M$$
$$h = \frac{V_{\text{dissolved}}}{1 \text{ cm}^2}$$



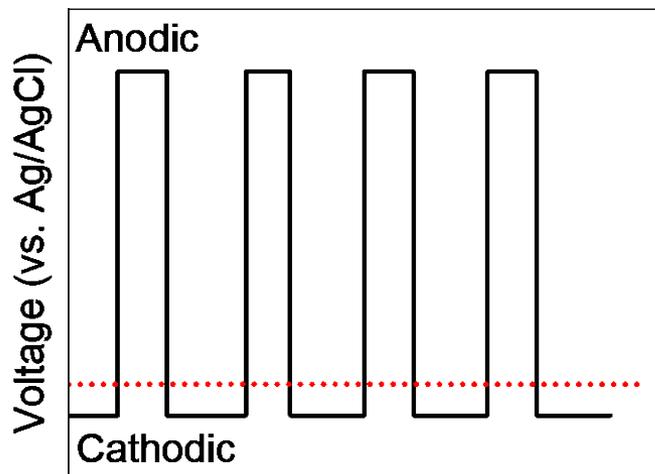
# Choosing Pulse Parameters

(Figure adapted from that published by Faraday Technologies)

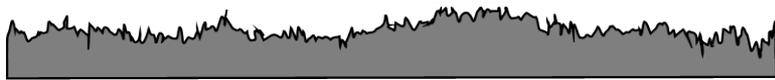
## Targetting Macro-asperities



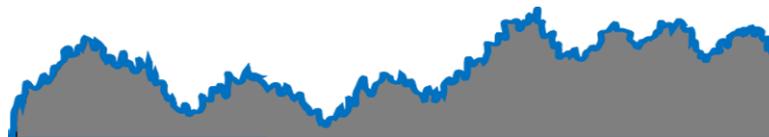
Short, intense  $t_{on}$  pulses generate a thin diffusion layer allowing for non-uniform smoothing, targeting macroasperities.



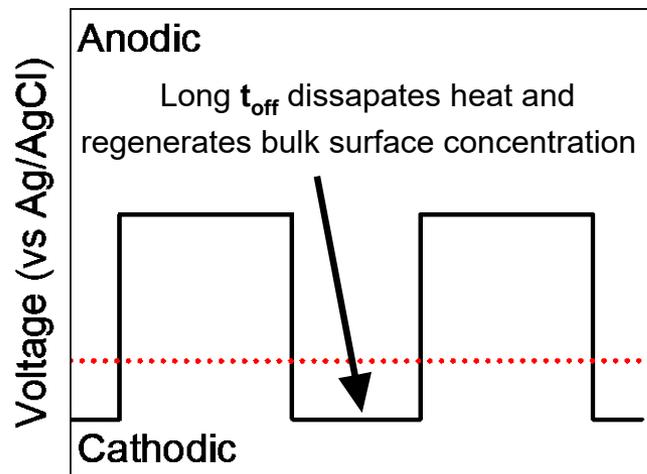
↓ Time (ms) ↓  
Macro-smoothed Surface



## Targetting Micro-asperities



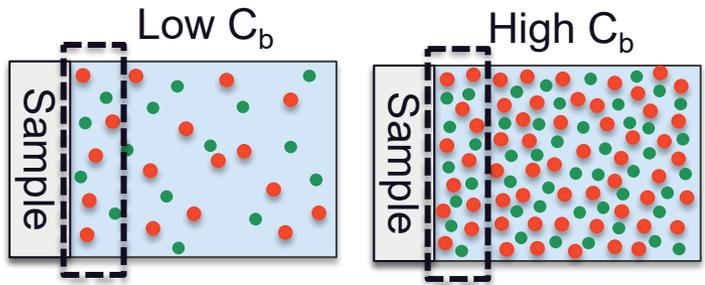
Long,  $t_{on}$  pulses generate a thick diffusion layer allowing for uniform smoothing, targeting microasperities. Lowering peak intensity lengthens transition time, maintaining a non-diffusion limited current distribution



↓ Time (ms) ↓  
Micro-smoothed Surface



# Choosing Pulse Width:



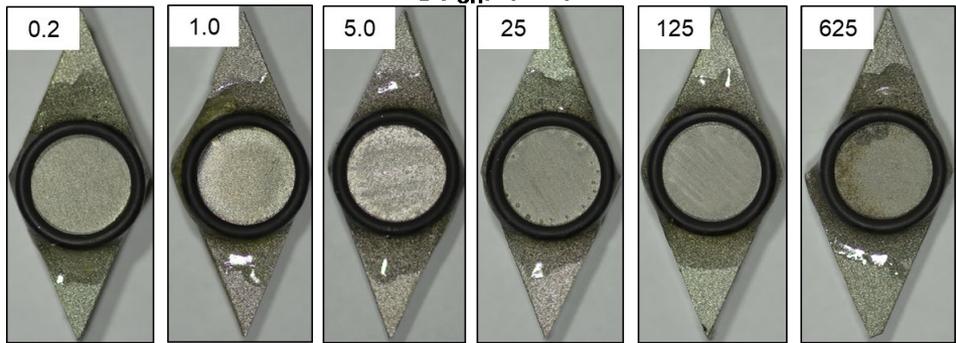
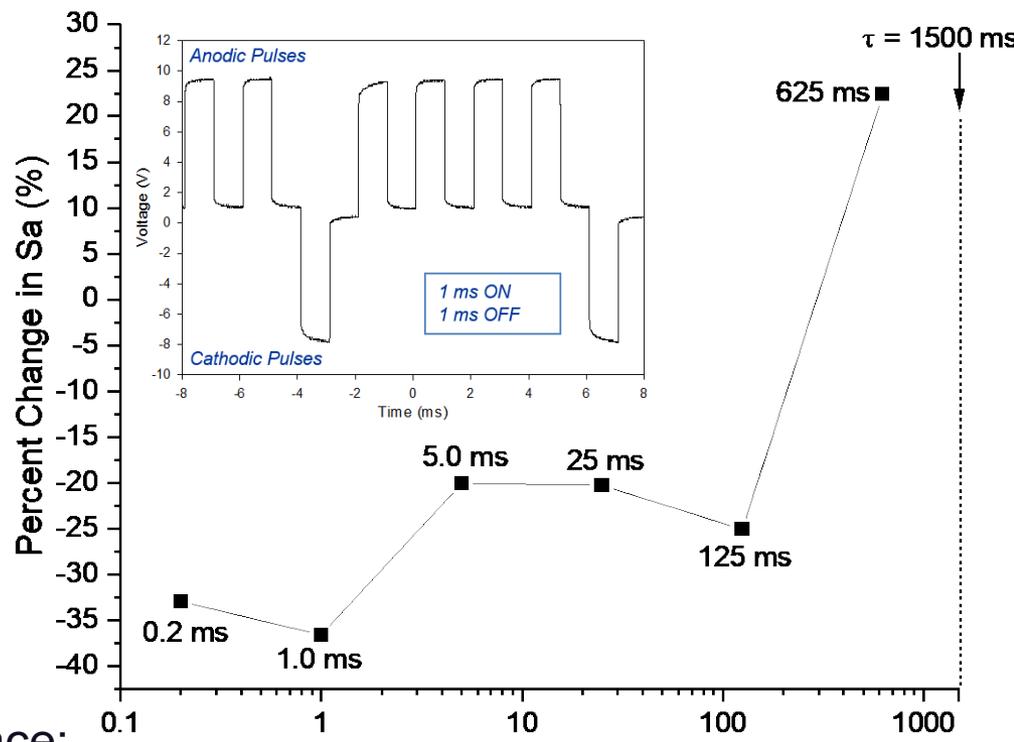
$$\tau = \frac{\pi \left( (nF)^2 C_b^2 D \right)}{4i_a^2}$$

$\tau$  (transition time):  
 How long at a given current does it take to consume all reagents at the surface?

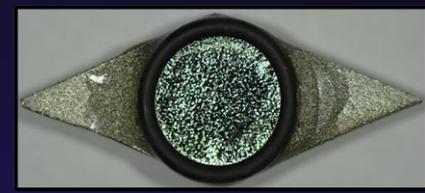
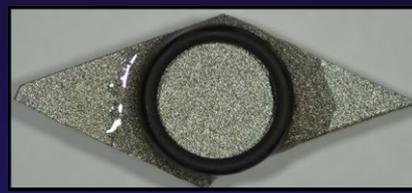
Factors outside mass transport alter surface:

1. Streaking at  $t_{on} > 1$  ms (bubbles)
2. Pitting/corrosion at  $t_{on} > 5$  ms
3. More severe corrosion at  $t_{on} > 125$  ms

For the following experiments,  
 $t_{on} = 1$  ms will be used



# Establishing a DC Basis for Comparison



## DC Electropolishing Experiment:

- Roughness, mass, and SEM before/after electropolishing
- Follow polishing protocol established by electrolyte manufacturer. (E-Polish Solutions)

90 °C

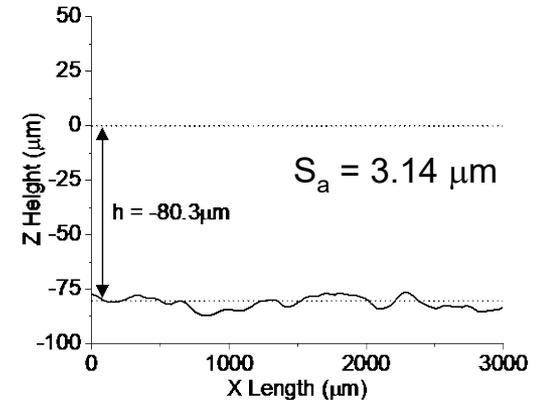
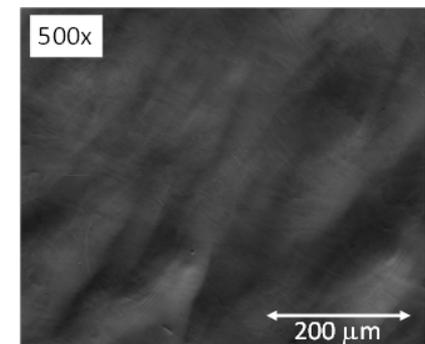
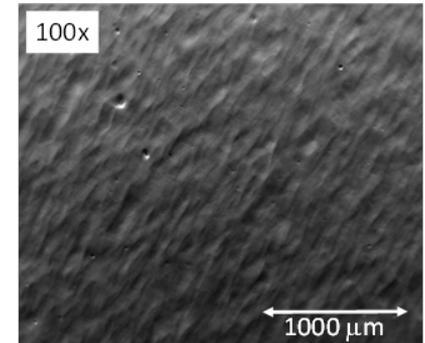
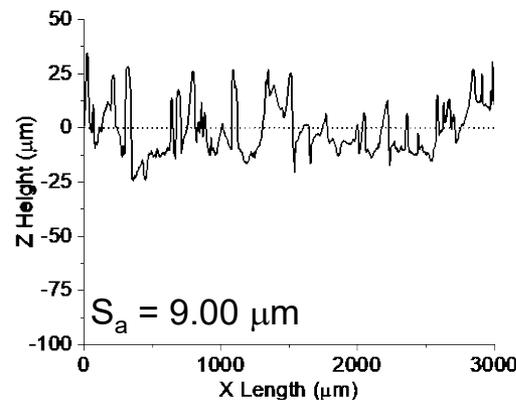
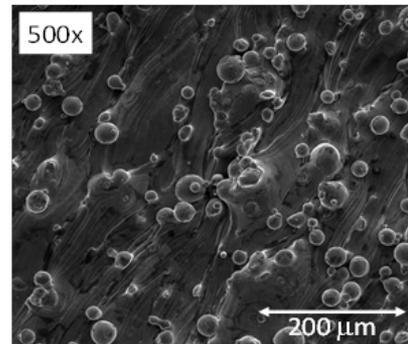
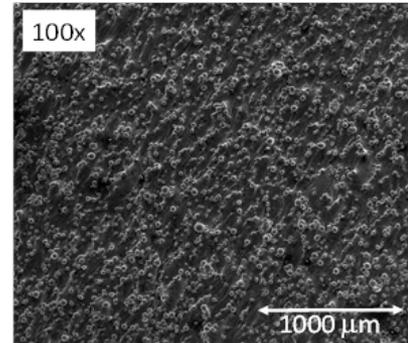
$H_3PO_4/H_2SO_4$

Current Density =  $0.936 \text{ A/cm}^2$

Coulombic Density =  $15 \text{ A}\cdot\text{min./cm}^2$

## Results:

Micro-asperities are removed,  
mirror-like finish,  $62 \text{ mg/cm}^2$   
material removed



# Pulse/Pulse Reverse Equivalent



## P/PR Electropolishing Experiment:

- Define duration at same peak current and coulombic density.

$$I_{eff} = I_{anode,peak}(DC_{anode,eff}) - I_{cathode,peak}(DC_{cathode,eff})$$

$$DC_{eff} = \frac{Dur_{electrode} \cdot t_{on,electrode}}{(Dur_{anode} \cdot t_{on,anode}) + (Dur_{cathode} \cdot t_{on,cathode})}$$

- Determine change in mass/roughness

## Conditions

2.5 °C

Na<sub>2</sub>SO<sub>4</sub>/NaCl/H<sub>2</sub>O

Agitation: None

Peak Current Density = 0.936 A/cm<sup>2</sup>

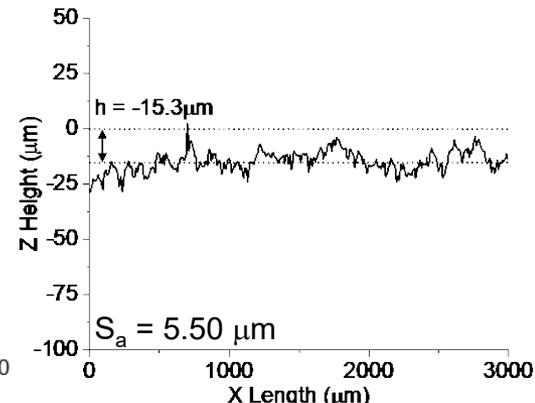
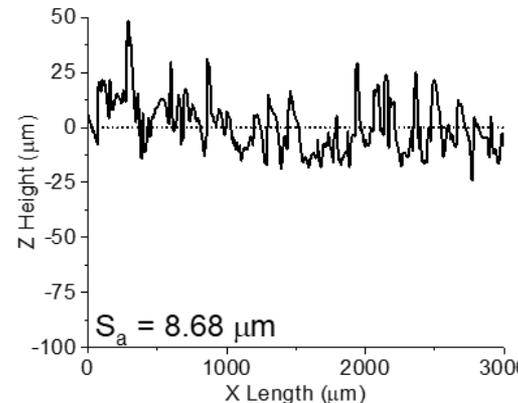
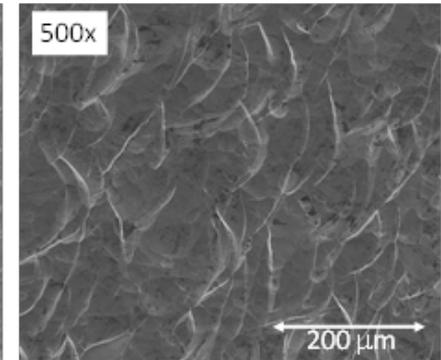
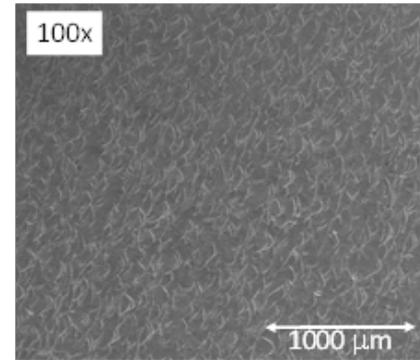
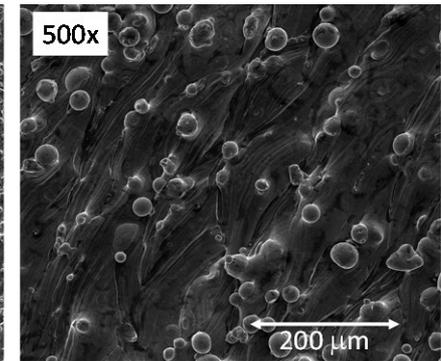
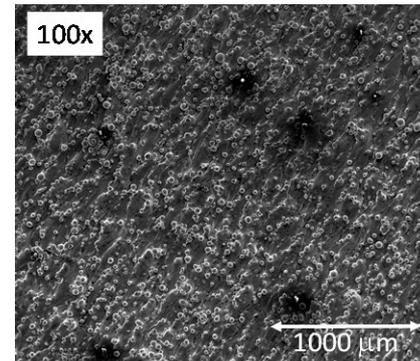
Coulombic Density = 7.5 A\*min./cm<sup>2</sup>

## Results:

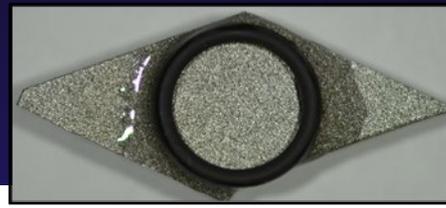
Considerably lower mass loss (12 mg/cm<sup>2</sup>)

Surface roughness not as improved vs DC

Fish scale-like microstructure

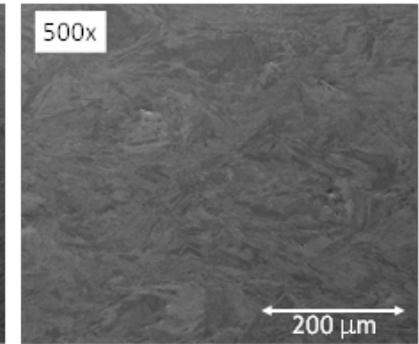
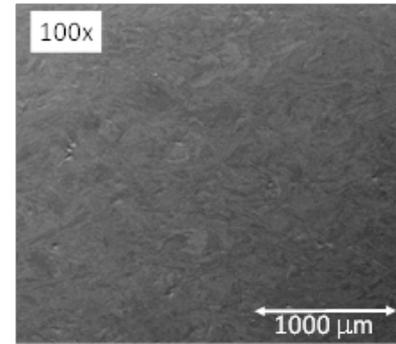
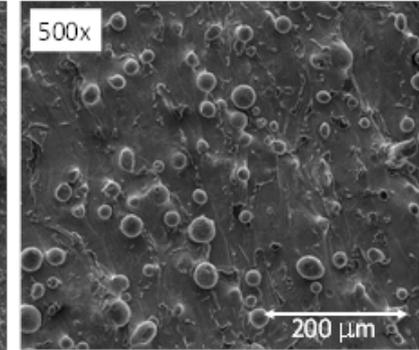
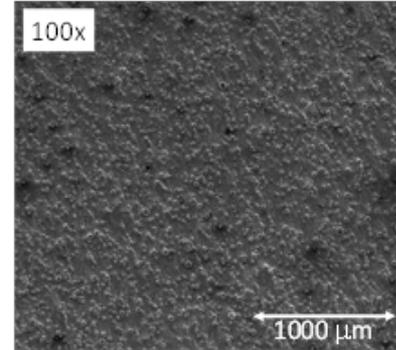


# Two-Bath Electropolishing Method



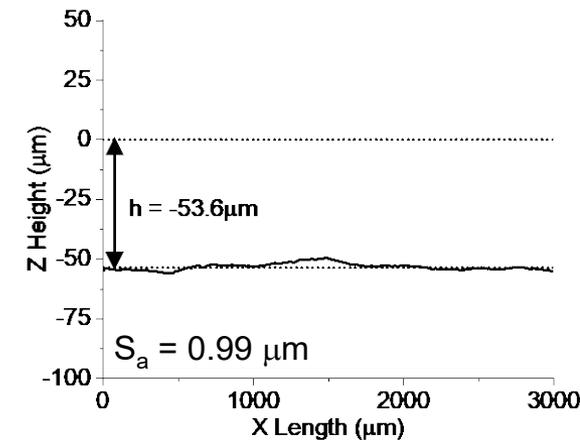
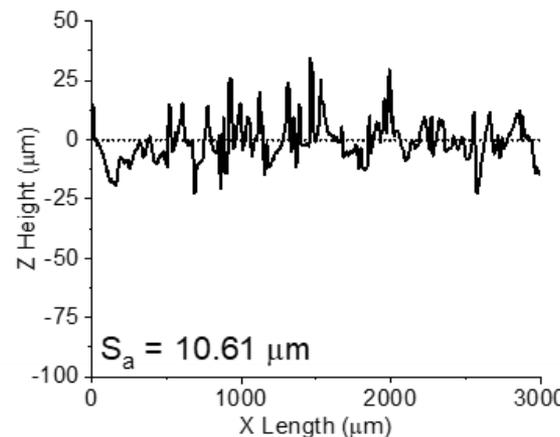
## Procedure:

1. P/PR (NaCl) at  $0.936 \text{ A/cm}^2$  up to  $7.5 \text{ A}\cdot\text{min/cm}^2$ .
2. Determine  $\Delta M/S_a$
3. DC at  $0.936 \text{ A/cm}^2$  an additional  $7.5 \text{ A}\cdot\text{min/cm}^2$  (15 total)
4. Determine  $\Delta M/S_a$



## Results:

- Less mass loss (35 mg) compared to full DC method
- Most improved surface roughness
- Macro- and Micro-smoothing



# Optimization of P/PR Sequence: Duration

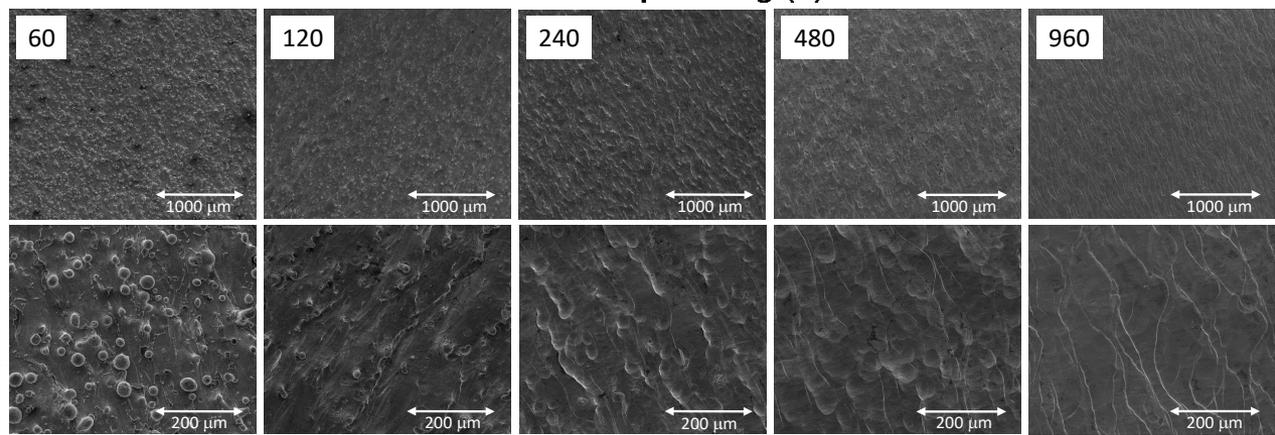
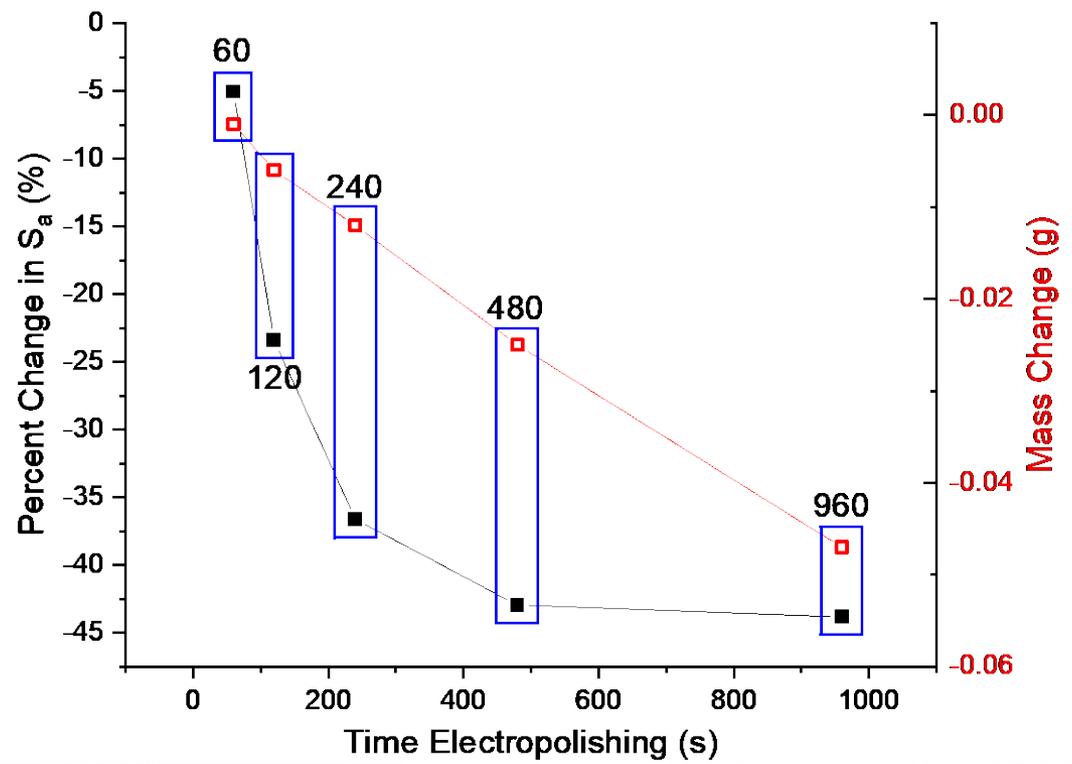
## Varying Coulombic Density:

How does surface roughness change as the surface is increasingly etched?

Separate samples were electropolished at increasing durations: microstructure,  $\Delta M$ , and  $\% \Delta S_a$  are tracked.

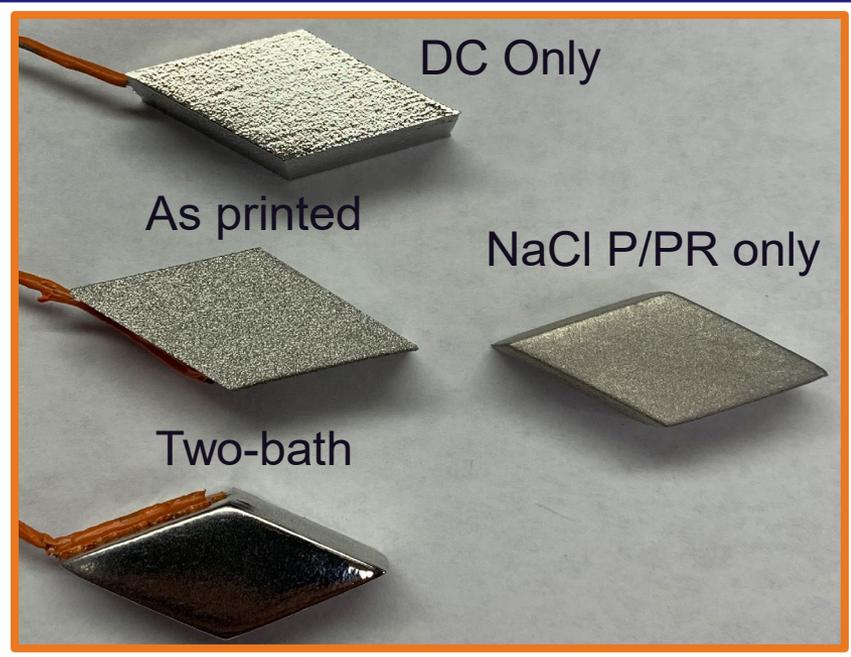
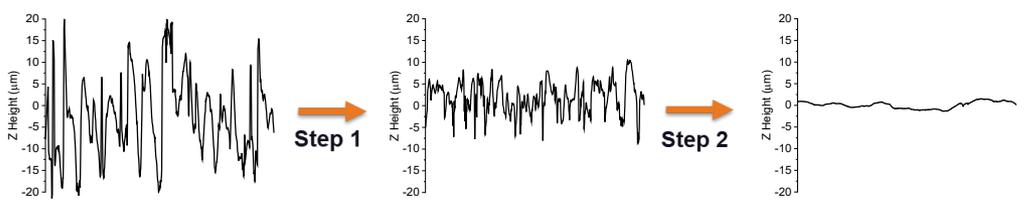
## Conclusions:

- 1. Mass decreases linearly with increasing coulombic density.
- 2. Surface roughness improves as a decaying function (diminishing returns)

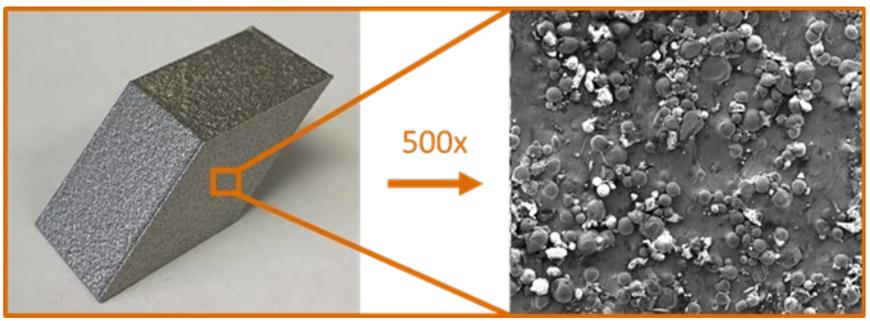


# 3D Components?

- Process can be scaled up with surface area
- Concerns with geometry changing
- Finite element modeling could be used to predict higher current density areas, use this to “over-print”



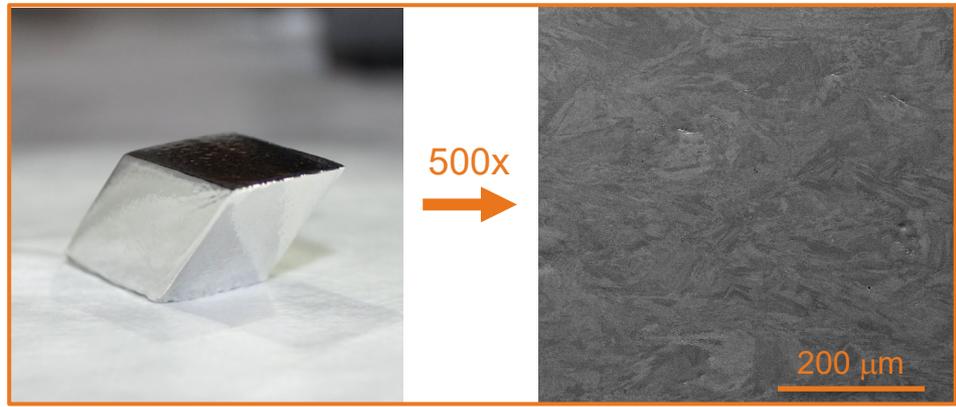
BEFORE



As-printed

$S_a = \sim 12 \mu\text{m}$

AFTER



Additive: Two-bath

$S_a = 0.99 \mu\text{m}$

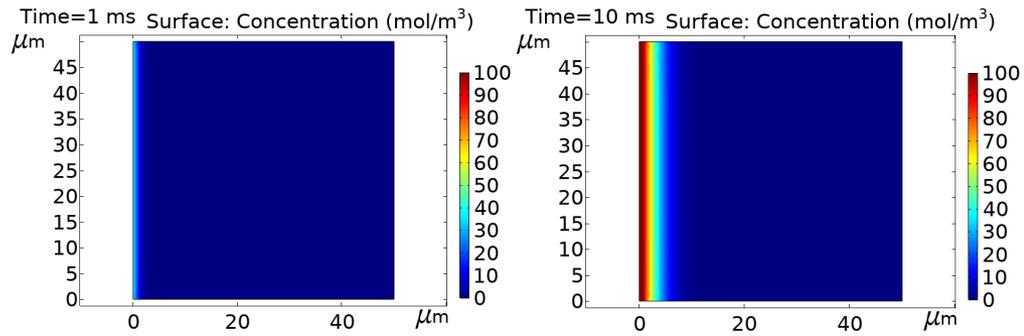
# Rationalizing the Electrochemistry:

## Physics to Consider:

➤ On-time: Nernst-Planck Equation:

$$J_i(x) = -D_i \frac{\partial C_i(x)}{\partial x} - \frac{z_i F}{RT} D_i C_i \frac{\partial \phi(x)}{\partial x} + C_i v$$

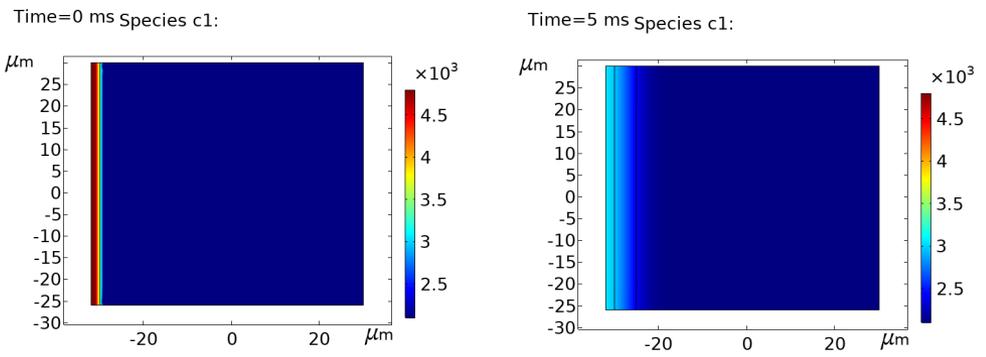
On-time also involves deforming geometry (i.e. dissolution) and current density distributions.



➤ Off-time: Fick's Law:

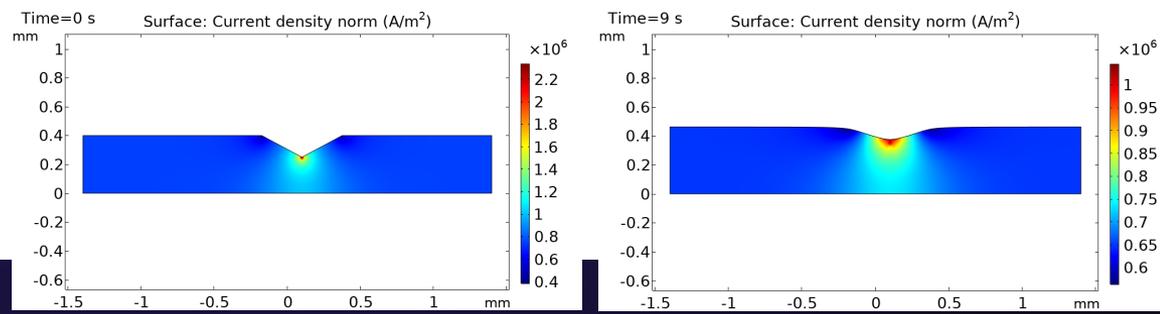
$$\frac{\partial C_i(x)}{\partial t} = D_i \frac{\partial^2 C_i(x)}{\partial x^2}$$

No electric fields or geometry changes



➤ Incorporating Geometry Change

Correlated with current distribution



# Conclusions

## DC Electropolishing:

- Limited to microsmoothing.
- Large mass loss/change in geometry.

## Pulse/Pulse Reverse:

- Currently limited to macrosmoothing; unable to get mirror-like finish.
- Greatly reduced mass change for equivalent coulombic density.

## Two-bath method:

- Currently able to macro- and micro-smooth full AM parts made of 316L Stainless steel.
- Less mass loss than traditional DC electropolishing, for equivalent coulombic density.

## Future Work:

- Design pulse sequence to address micro-smoothing, i.e. single-bath method.
- Scale up to complex geometry (lattices)
- Extend technique to alternative materials (e.g. titanium, aluminum, etc).

# Questions?